

Modeling of polycrystalline materials using a two-scale FE-FFT-based simulation approach

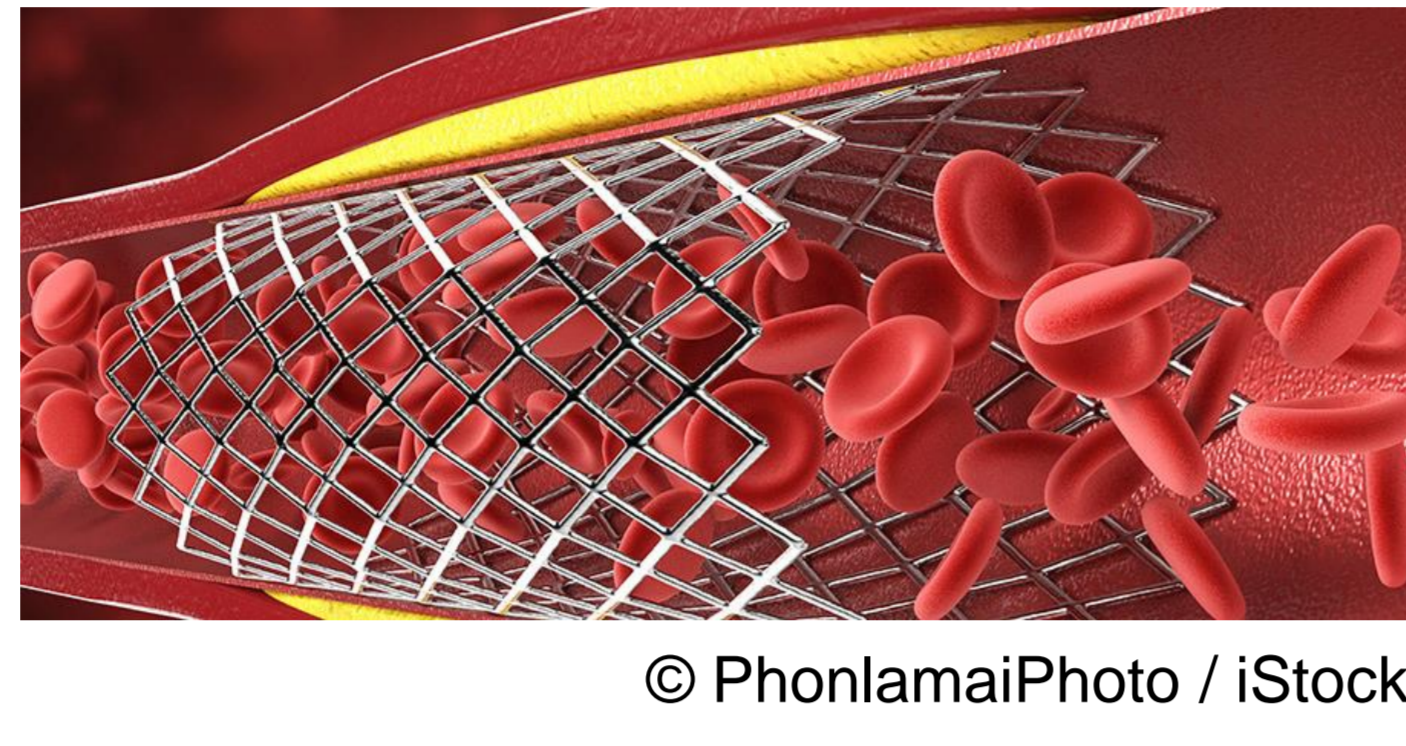
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Motivation

Polycrystalline materials used in engineering applications



Automotive industry



Medical applications

Desired material properties

- ▶ High strength
- ▶ Long durability
- ▶ Light weight
- ▶ Wear resistance

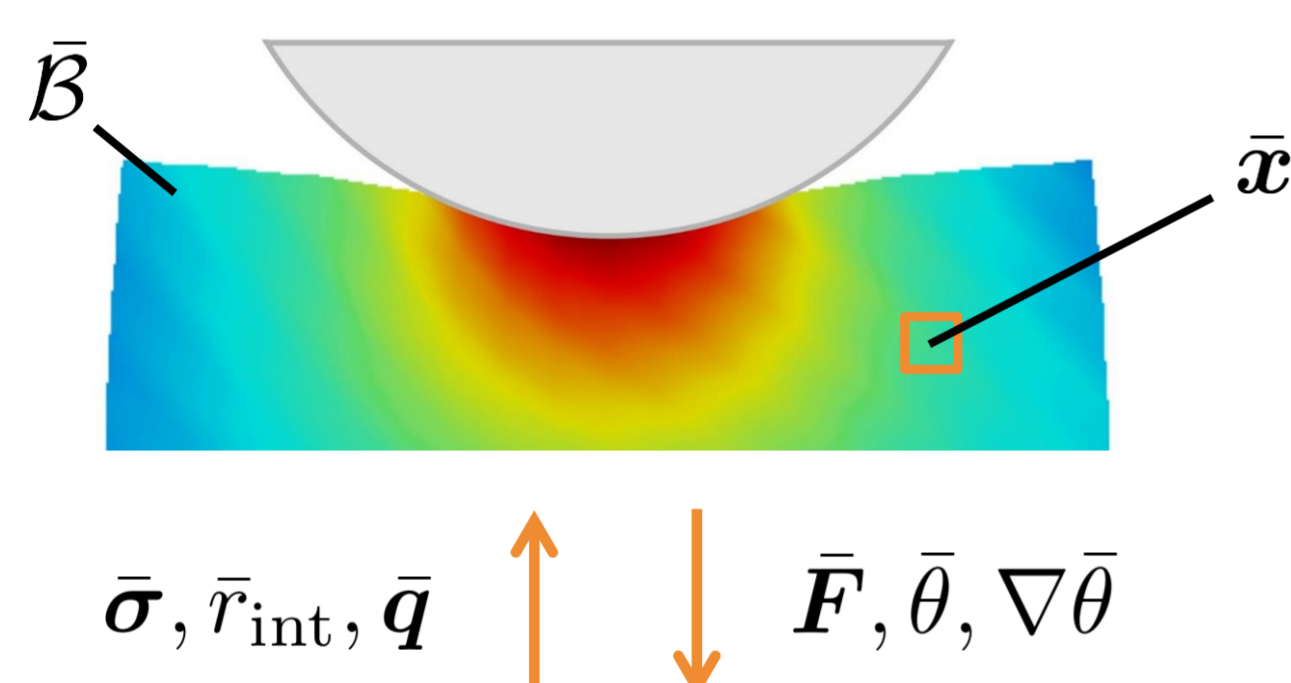
Development of optimized components

- ▶ Reduced material consumption
- ▶ Targeted adjustment of functional properties

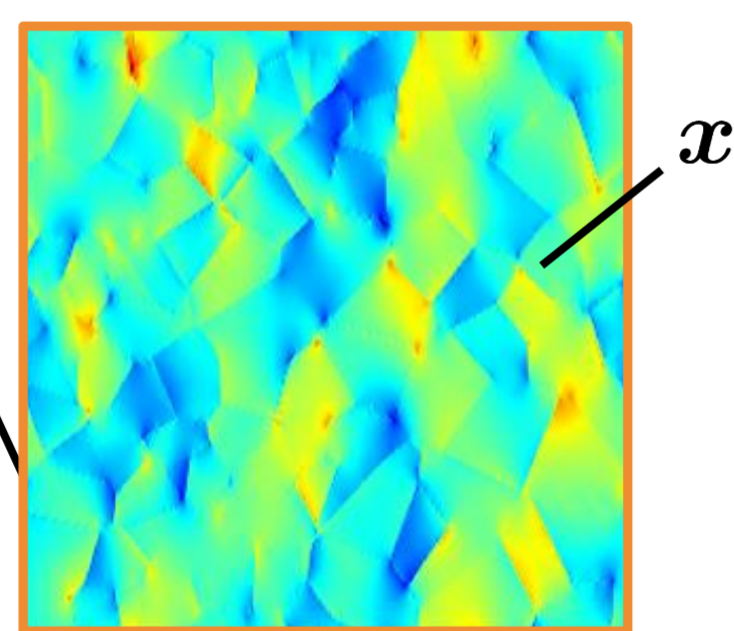
- ▶ Prediction of material behavior using a two-scale thermo-mechanically coupled FE-FFT-based simulation approach

Two-scale FE-FFT-based simulation

Homogeneous macroscale



$\bar{\sigma}, \bar{r}_{int}, \bar{q}$ $\bar{F}, \bar{\theta}, \nabla \bar{\theta}$



Heterogeneous microscale

- $(\bar{\bullet})$: Macroscopic quantity
- (\bullet) : Microscopic quantity
- x : Position vector
- F : Deformation gradient
- σ : Cauchy stress
- θ : Temperature
- $\nabla \theta$: Temperature gradient
- r_{int} : Internal heat sources
- q : Heat flux

Numerical methods [1,2,3]

- ▶ Finite element (FE) method on macroscale
- ▶ Fast Fourier transform (FFT)-based simulation technique on microscale

Microscopic FFT-based solution approach

Governing equations in Fourier space

- ▶ Mechanical boundary value problem

$$\hat{F}(\xi) = \begin{cases} -\hat{\Gamma}^0(\xi) : \hat{\tau}(\xi) & \text{for } \xi \neq 0 \\ \bar{F} & \text{for } \xi = 0 \end{cases}$$

- ▶ Thermal boundary value problem

$$\nabla \hat{\theta}(\xi) = \begin{cases} \hat{r}_{int}(\xi) \xi & \text{for } \xi \neq 0 \\ \nabla \bar{\theta} & \text{for } \xi = 0 \end{cases}$$

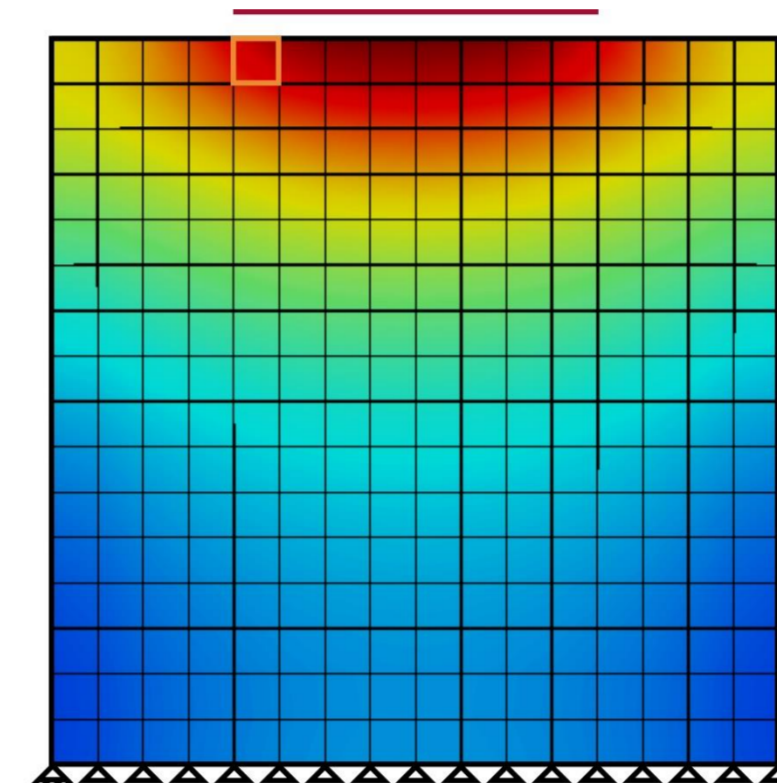
- $(\hat{\bullet})$: Quantity in Fourier space
- ξ : Fourier mode
- Γ^0 : Green's operator
- κ : Heat conductivity

Structural examples

Multi-physically coupled two-scale simulations

- ▶ Modeling the thermo-mechanically coupled material behavior of copper [4,5]

Heating $\Delta \bar{\theta} = 200 \text{ K}$

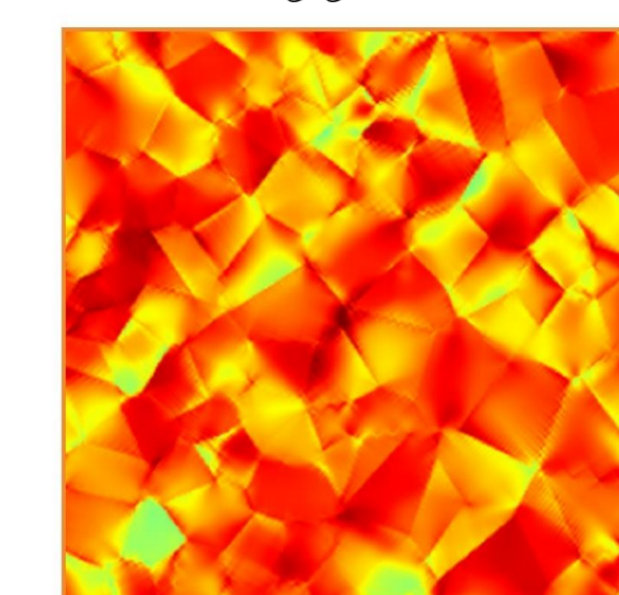


$\overline{LE}_{yy} [\%]$

0.58

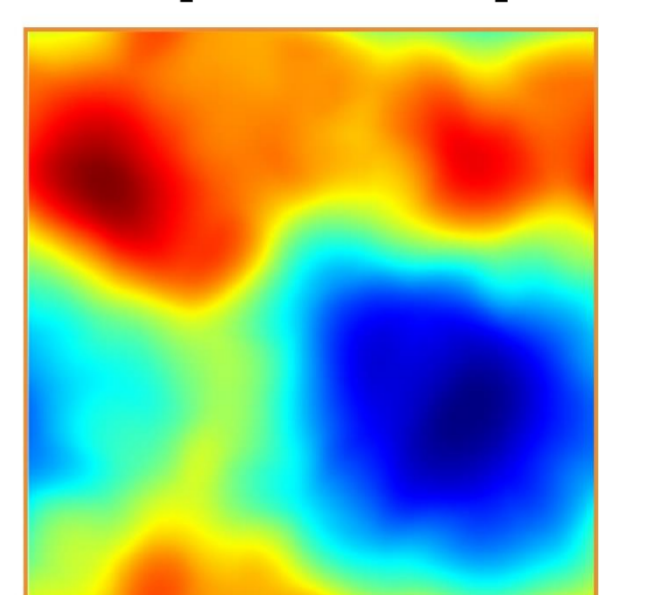
0

$E_{yy} [\%]$



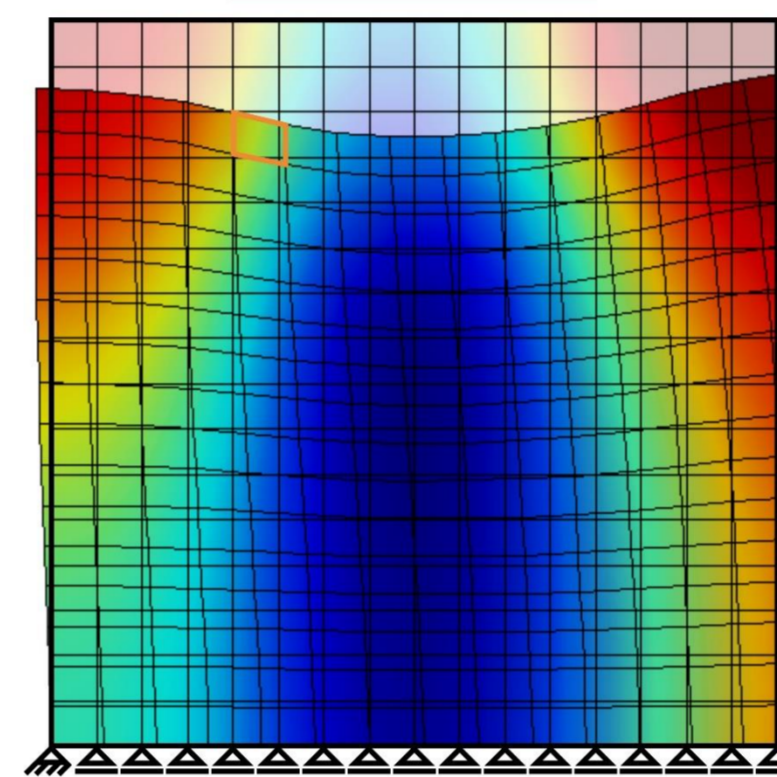
0 0.74

$\tilde{\theta} [\cdot 10^{-8} \text{ K}]$



-7.6 7.2

Line force $\bar{t} = 160 \text{ MPa}$

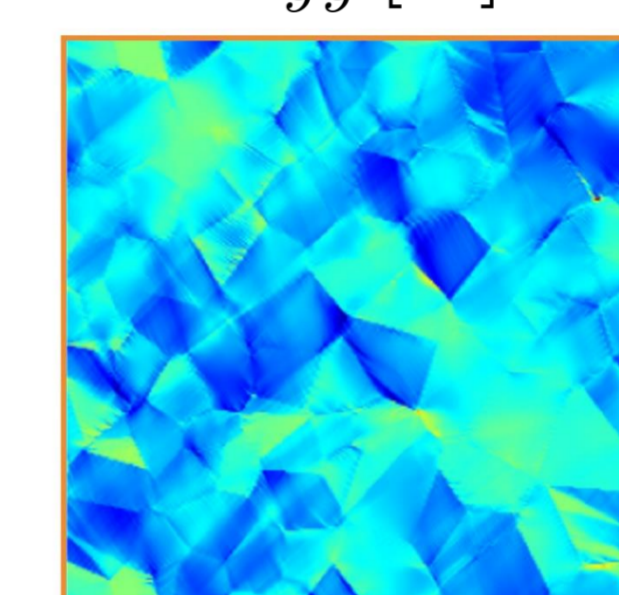


$\overline{LE}_{yy} [\%]$

-5.5

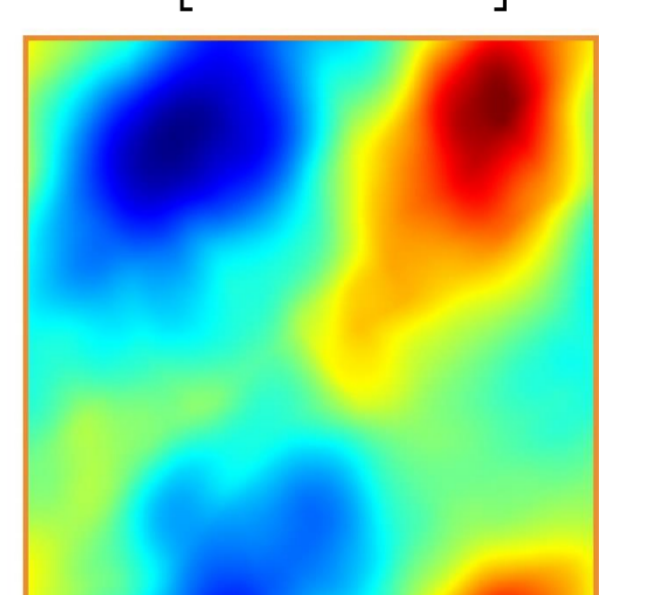
-17.9

$E_{yy} [\%]$



-27.0 25.0

$\tilde{\theta} [\cdot 10^{-7} \text{ K}]$



-2.2 2.6



Heating

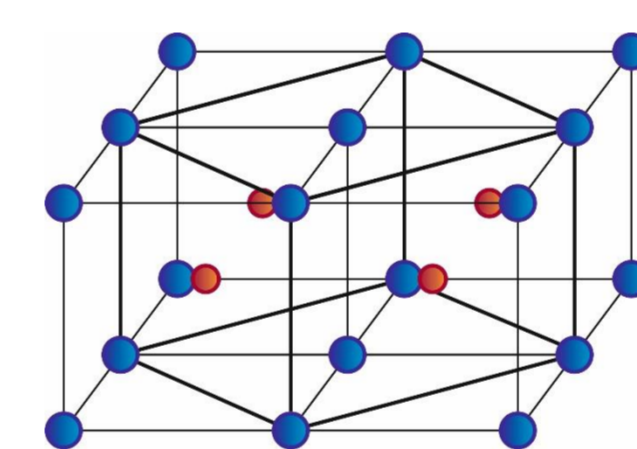


Line force

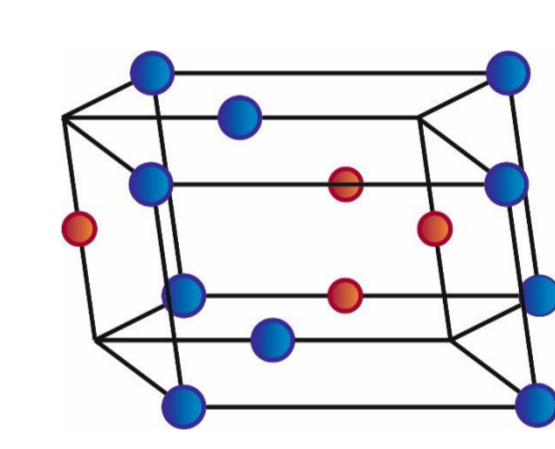
LE : Logarithmic strain
E : Green-Lagrange strain
 $\tilde{\theta}$: Fluctuating temperature field

Two-scale simulations of shape memory alloys

- ▶ Modeling stress-induced phase transformations between austenite and martensite [6,7]

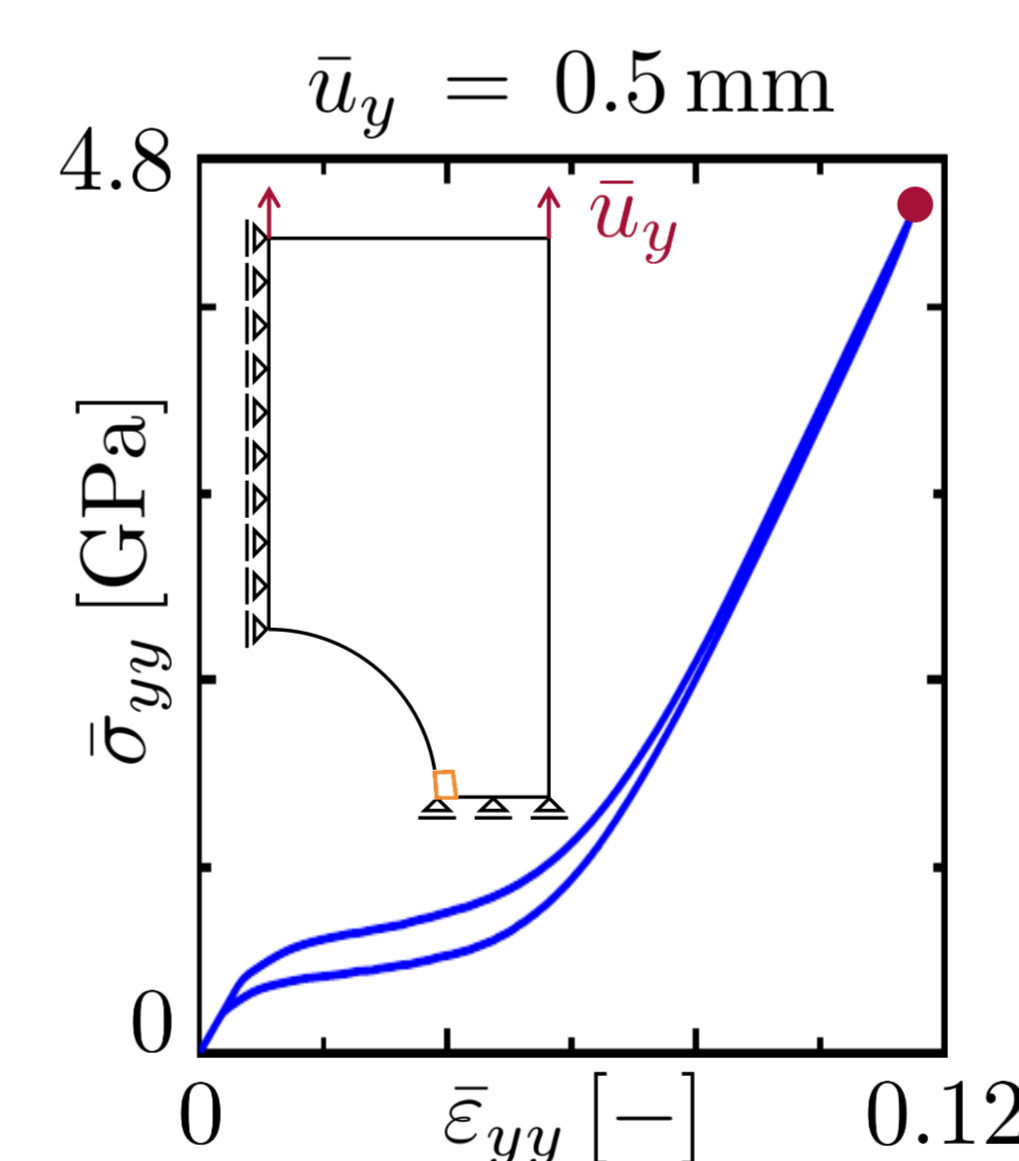


Austenitic lattice



Martensitic lattice

- ▶ Pseudoelastic material behavior



$\bar{u}_y = 0.5 \text{ mm}$

$\bar{\sigma}_{yy} [\text{GPa}]$

4.8

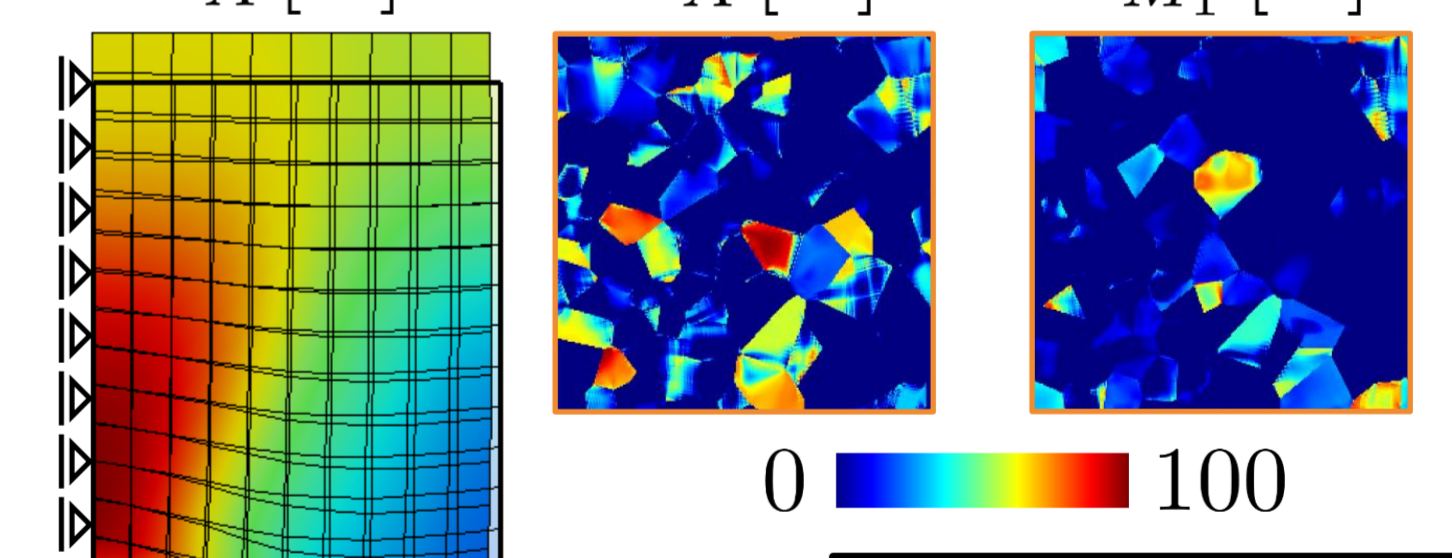
0

0.12

$\bar{\varepsilon}_{yy} [-]$

- ▶ Martensitic phase transformation

$\bar{\lambda}_A [\%]$ $\lambda_A [\%]$ $\lambda_{M_1} [\%]$



0 100

100 0

λ_i : Volume fraction of phase i

Evolution of martensitic phase transformations over complete simulation time

Evolution of martensitic phase transformations over complete simulation time

Evolution of martensitic phase transformations over complete simulation time

References

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